

# Operation on Ammonia and Hydrogen at the Rough Limit

NH3Car

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# Outline

- Combustion Equation
- Engine and Operating Parameters
- Predictions Based on Open Flame Experiments
- $\text{H}_2/\text{NH}_3$  Rough Limit
- Thermal Efficiency Max and Rough Limit Min
- Conclusions

# Combustion Equation

- $$(0.79 \text{ N}_2 + 0.21 \text{ O}_2) + 0.42b \text{ H}_2 + 0.28(1-b) \text{ NH}_3 \Rightarrow (0.93 - 0.14b) \text{ N}_2 + 0.42 \text{ H}_2\text{O}.$$
- Hydrogen is the combustion promoter.
- $b$  = Chemical Equivalence basis hydrogen fraction.  
 $0 \leq b \leq 1$ . Also fraction of hydrogen not as ammonia.  
Approximates case of side stream cracking.
- Exact for case of auxiliary high pressure hydrogen tank instead of cracker.

# Experimental Engine and Equipment

- CFR Engine
- Variable compression ratio 8:1 to 16:1.
- Operation up to normally aspirated, WOT
- Restricted speed to 1600 RPM.
- Cylinder pressure monitored with sensor
- Single cylinder = 0.625 liters



# Ammonia/Propane Open Flame

- Open Flame Experiments -> One Condition, One Fuel Mix



Propane Only



Ammonia and Propane



Inadequate Propane

- Minimum HC energy fraction = 40-50% at  $P = 1$  atm,  
 $T_o$  = room temperature
- Gasoline Input at Rough Limit for Engine  $\sim 600$  J/L
- Cooked a turkey with Ammonia and Propane

# Ammonia/Hydrogen Open Flame

- Make a Prediction about H<sub>2</sub> Rough Limit Behavior



28% H<sub>2</sub>/72% NH<sub>3</sub> by volume.      18% H<sub>2</sub>/82% NH<sub>3</sub> by volume.

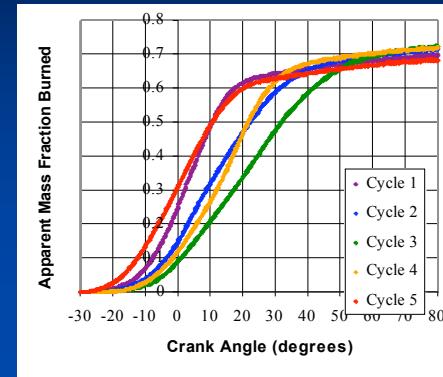
- Minimum Hydrogen Fraction as Hydrogen  $\sim 20\%$  at  $P = 1 \text{ atm}$ ,  $T_o = \text{room temperature}$
- Estimated Rough Limit Rescaling Factor  $\sim 1/2$
- Estimated Rough Limit Hydrogen Input  $\sim 300 \text{ J/L}$

# Rough Limit at 1600 RPM for Gasoline

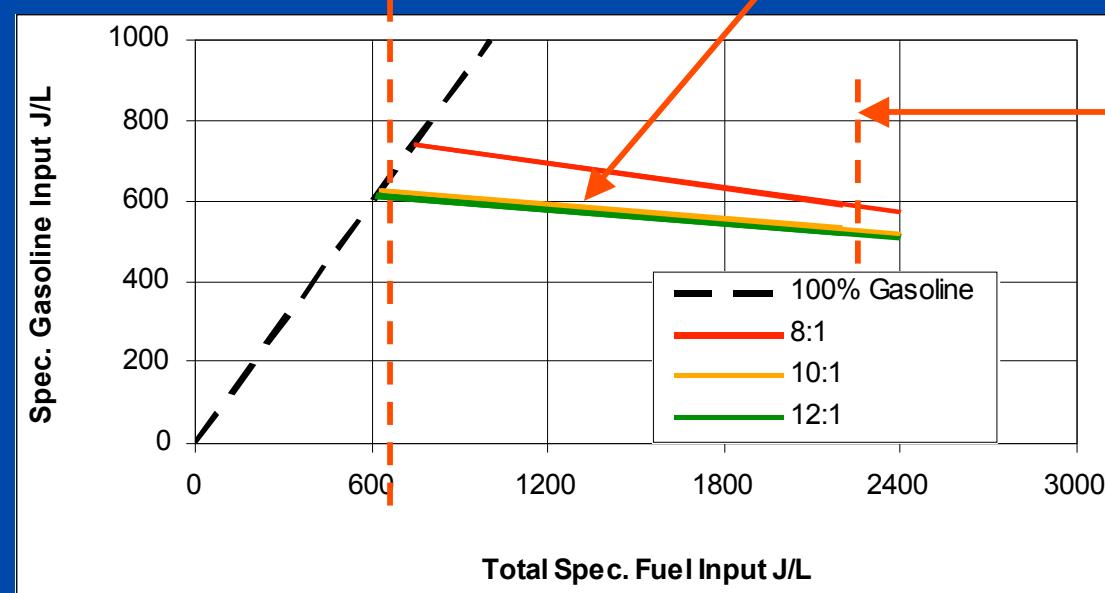
100% Gasoline Rough Limit  
occurs near Idle

Could use Gasoline at Idle for  
all loads > Idle

Rough  
Limit  
Behavior



Increasing  
combustion  
promoter  
input per  
cycle



Increasing  
Load

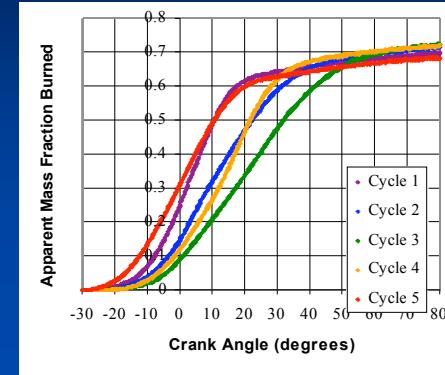
Normally  
Aspirated  
WOT

# Rough Limit at 1600 RPM for Hydrogen

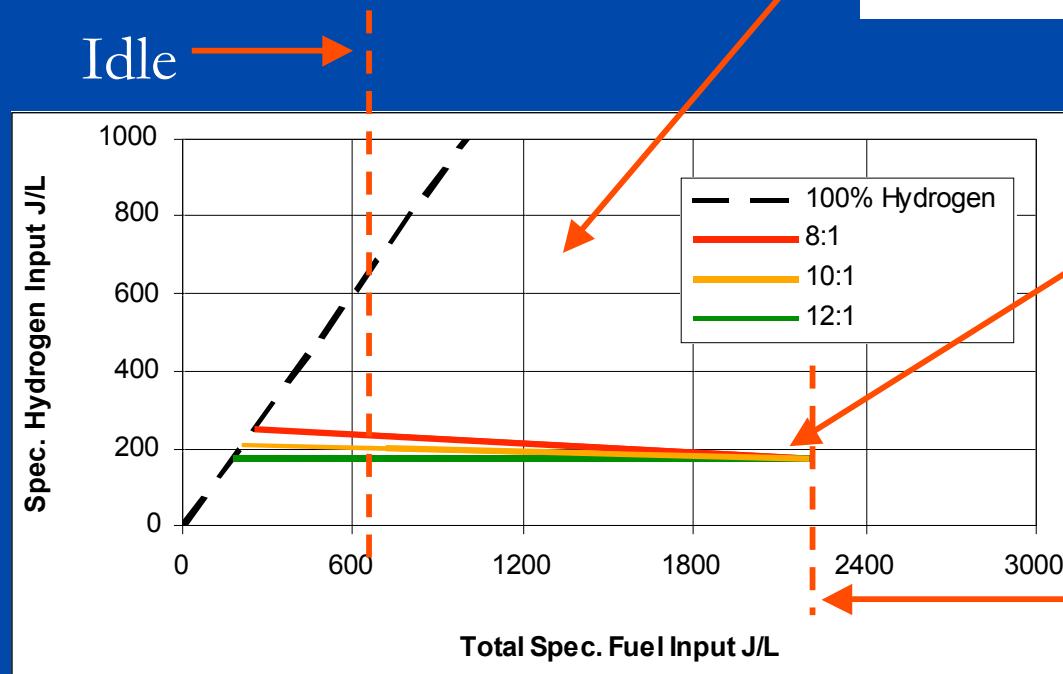
100% H<sub>2</sub> Rough Limit occurs substantially below Idle

Rough Limit Behavior

Could use Rough Limit at Idle for all loads > Idle



Increasing combustion promoter input per cycle

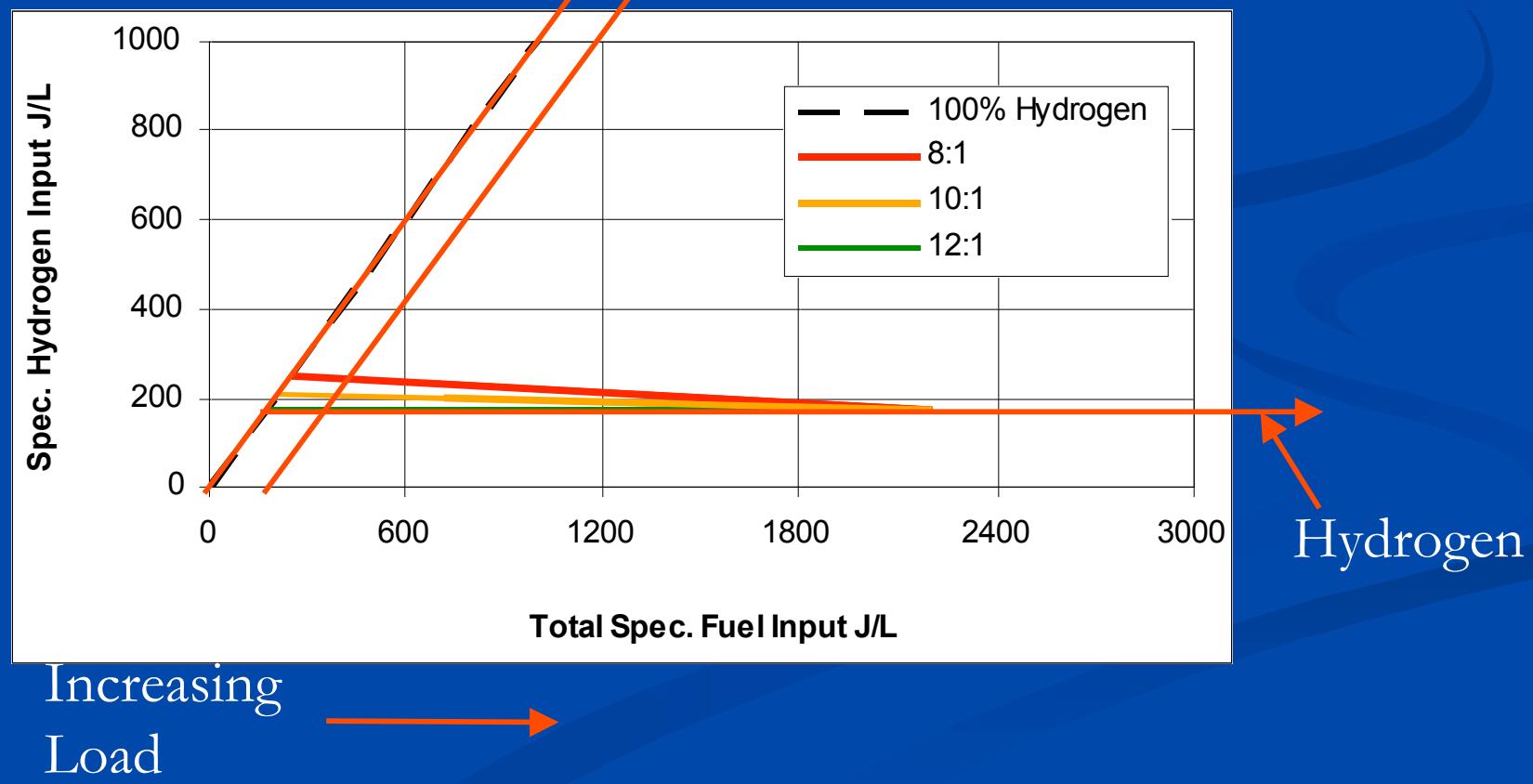


Increasing Load

70% H<sub>2</sub> for Rough Lim.  
7-10% for constant H<sub>2</sub>

Normally Aspirated WOT

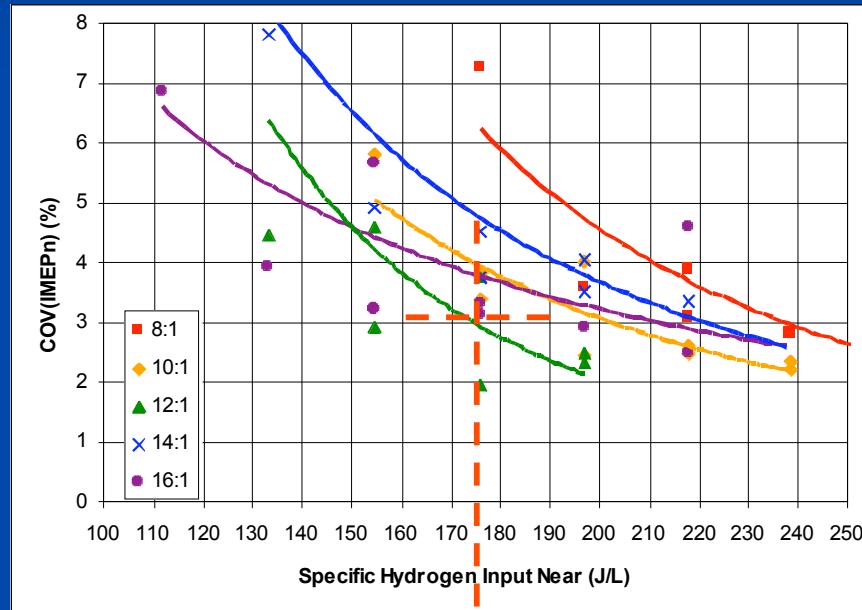
# Rough Limit at 1600 RPM, 12:1 for Hydrogen



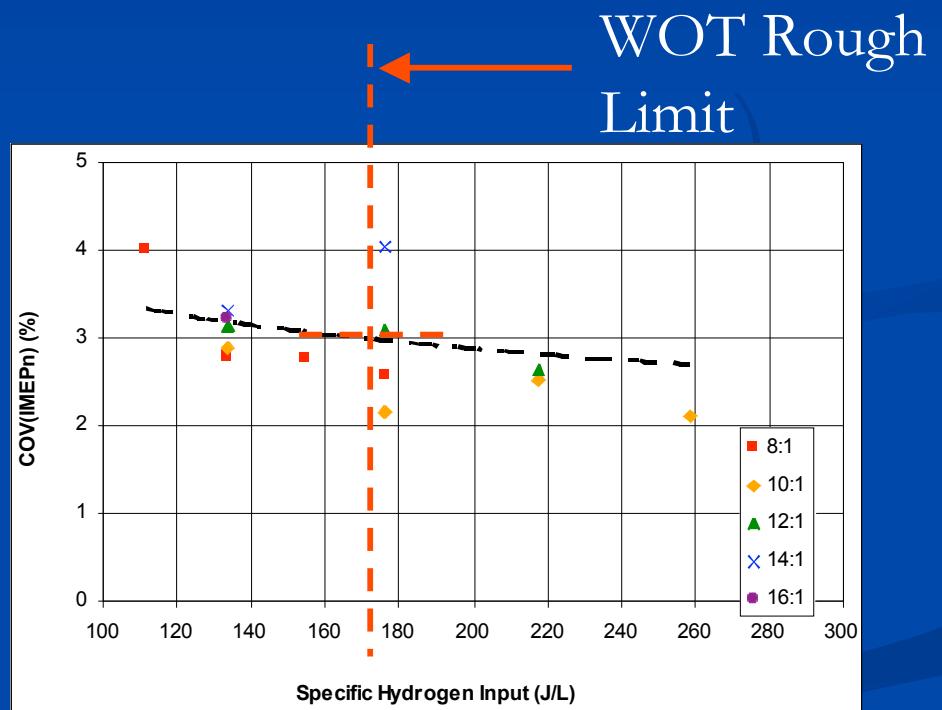
# Rough Limit = 3% COV(IMEP<sub>n</sub>)

## Rough Limit For Hydrogen

Near Idle



WOT



12:1 Rough  
Limit near Idle

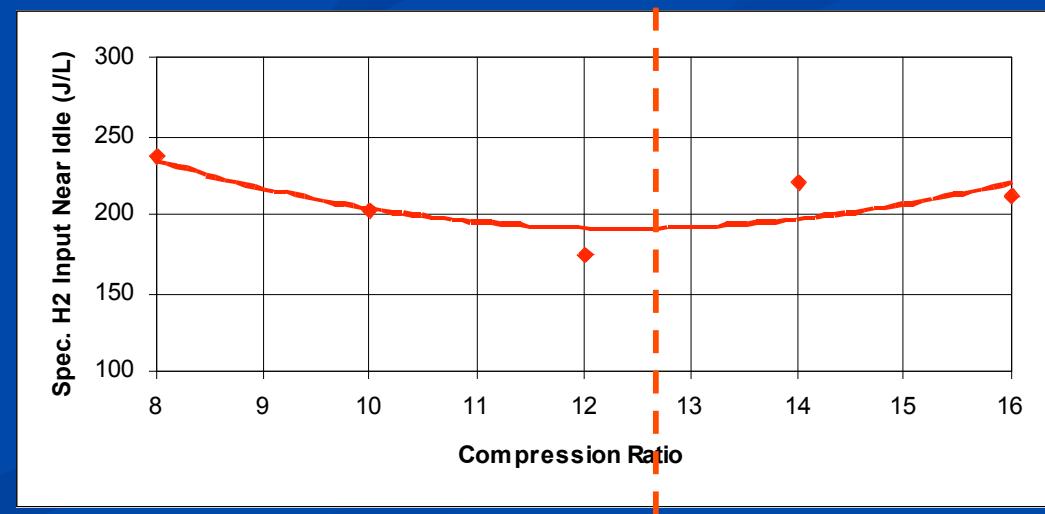
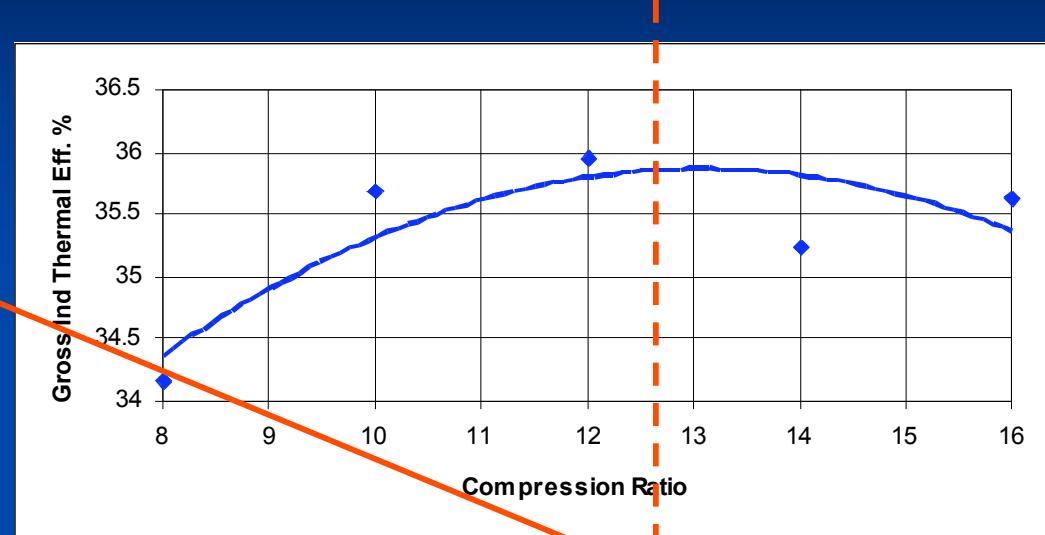
# Rough Limit and Efficiency Trends ~ Idle

Rough Limit Promoter  
Input Minimum and  
Efficiency Maximum  
Occur at Same  
Compression Ratio!

Rough Limit Hydrogen  
Input  $\sim 200$  J/L

For Gasoline, this was  
 $\sim 600$  J/L

Rough Limit Rescaling  
Factor = 1/3



- The ammonia fueled engine works.
- It can be made to work with gasoline for partial operation on ammonia, or hydrogen for ammonia-only operation.

- 100 Billion gallons of gasoline/year equivalent for U.S. = 374 Gigawatts = 694 million tons NH<sub>3</sub>/year.

# Conclusions

- There is a compression ratio at which the combustion promoter requirement is minimized, and in this case it is the same compression ratio for which efficiency is maximized, in this case about 12:1.
- The required ammonia decomposition fraction is not constant. The hydrogen input/cycle  $\sim$  constant.
- The specific promoter input at the rough limit near idle is about 200 J/L for hydrogen, whereas for gasoline it was about 600 J/L. The hydrogen partial energy input at the rough limit is about 1/3 of that of gasoline.
- The required % decomposition of ammonia at WOT should be about 7-10%.

