

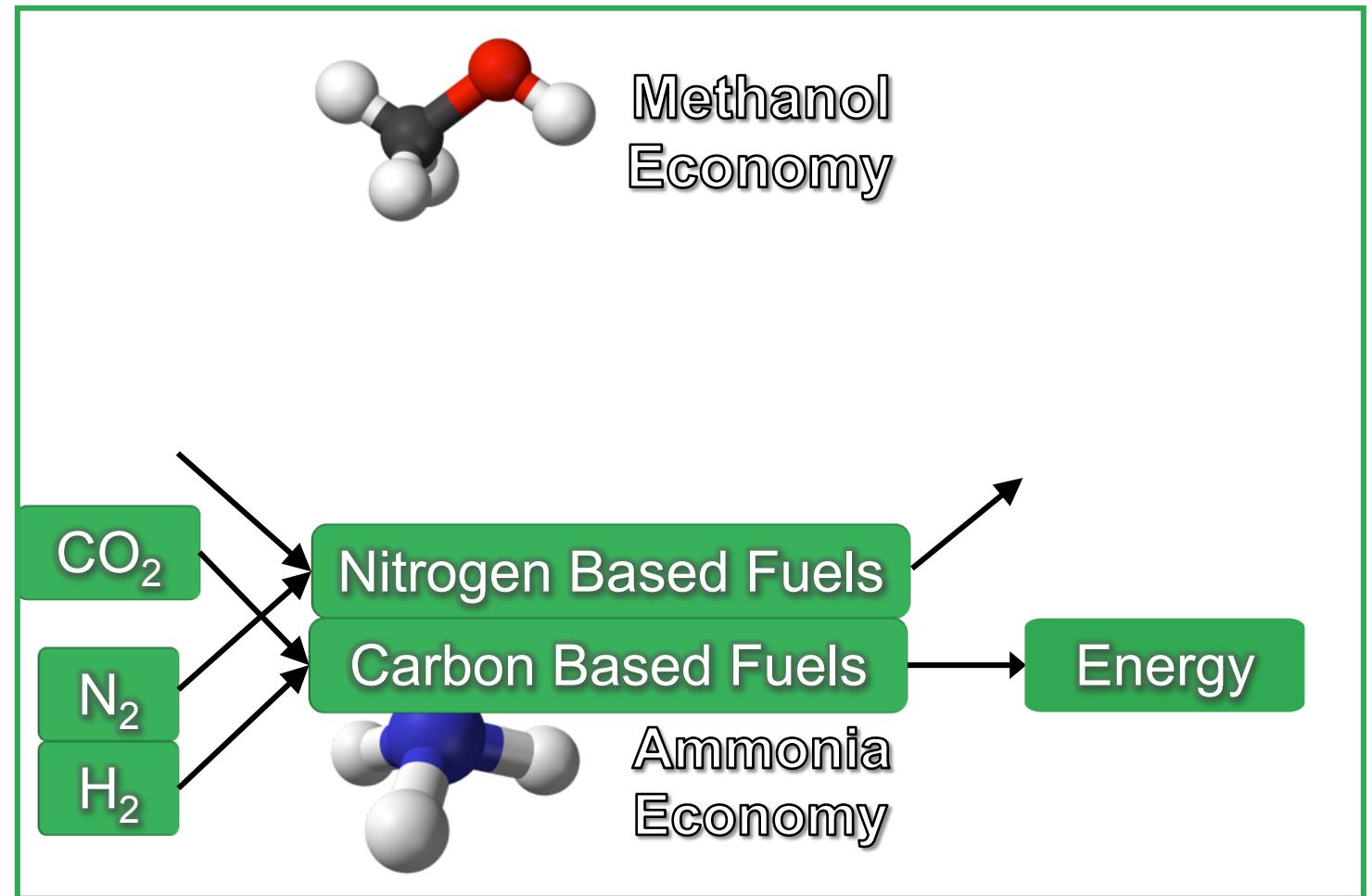
# Nitrogen-based Fuels: Renewable Hydrogen Carriers

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# Motivation

- Economic renewable  $H_2$  is getting closer
- $H_2$  is incompatible with large scale fuel transport infrastructure
- Chemical fuels are attractive  $H_2$  carriers since they are safer and easier to transport
- Chemical fuels offer higher volumetric energy densities than pure  $H_2$

But what fuels can we choose from?



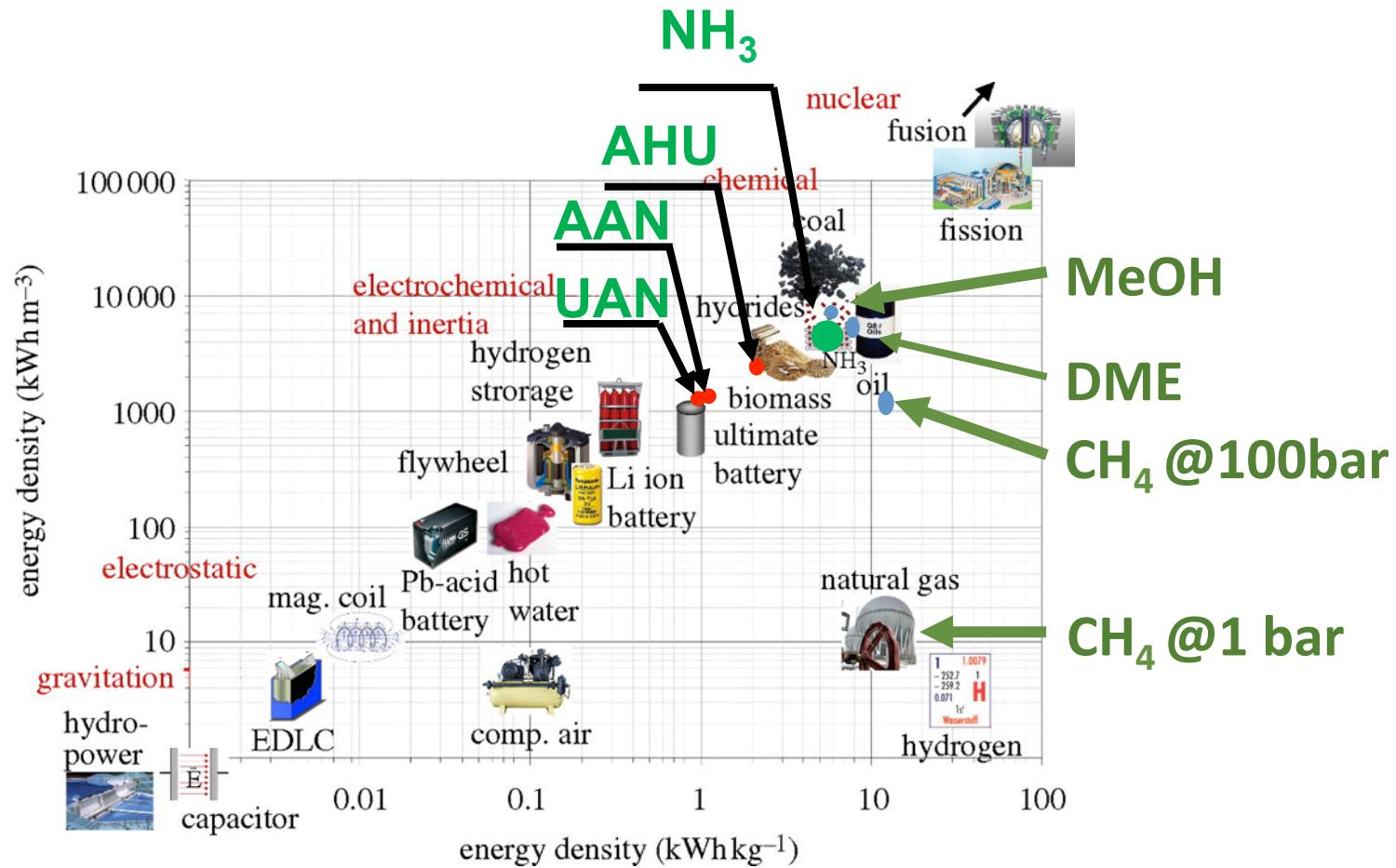
# Motivation

- Synthetic fuels from  $N_2$  &  $H_2$  can be gases, liquids or solids.
- $N_2$ -based fuels are competitive with carbon-based fuels.

## Energy Density?

## Any Special Applications?

- High pressure gas (e.g. EOR)
- Ammonia to power: ammonium nitrate in-situ ignition agent.

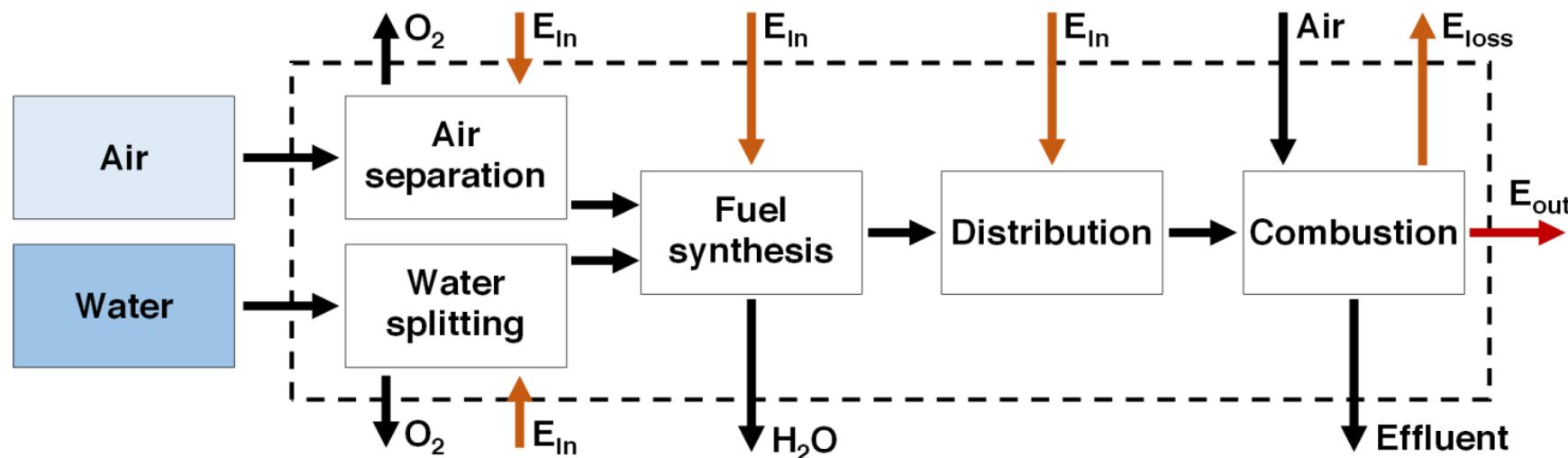


R. Lan et al., *Int. J. Hydrogen Energy*, **37**, 1482-1494, 2010.

# Feasibility of Nitrogen-based Fuels

## Power to Fuel to Power Analysis – PFP index

For any synthetic fuel the ratio of the useful energy output and the synthesis energy from stock materials can be calculated giving rise to the PFP index:



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$$PFP \uparrow atm = (energy\ density) \cdot \eta \downarrow combustion / (water\ splitting) + (air\ separation) + (synthesis) + (distillation)$$

# Feasibility of Nitrogen-based Fuels

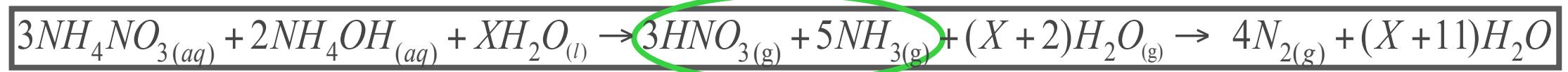
## Power to Fuel to Power Analysis – PFP index

For any synthetic fuel the ratio of the useful energy output and the synthesis energy from stock materials can be calculated giving rise to the PFP index:

Fuel	Air Separation (CQ/N <sub>2</sub> ) (GJ ton <sup>-1</sup> )	Water splitting (GJ ton <sup>-1</sup> )	synthesis energy (GJ ton <sup>-1</sup> )	Distribution (GJ ton <sup>-1</sup> )	Energy Density (HHV) (GJ ton <sup>-1</sup> )	Combustion efficiency	PFP index
CH <sub>4</sub>	18.1	90.8	1.2	1.51	55.5	54%	27%
MeOH	9.1	34.1	4.8	0.13	23.7	54%	27%
DME	12.6	47.4	8.7	0.15	31.7	50%	23%
NH <sub>3</sub>	0.18	32.1	1.6	0.19	22.5	53%	35%
Aq. AHU	2.56	14.6	1.5	0.10	9.2	50%	27%
Aq. ANA	0.06	115	0.9	0.08	3.7	47%	14%
Aq. UAN	0.79	10.9	1.3	0.07	3.3	48%	12%

# Effect of $\phi$ on AAN ignition

- Ammonium nitrate is a net oxidizer, decomposing into ammonia (reducer) and nitric acid (oxidizer)



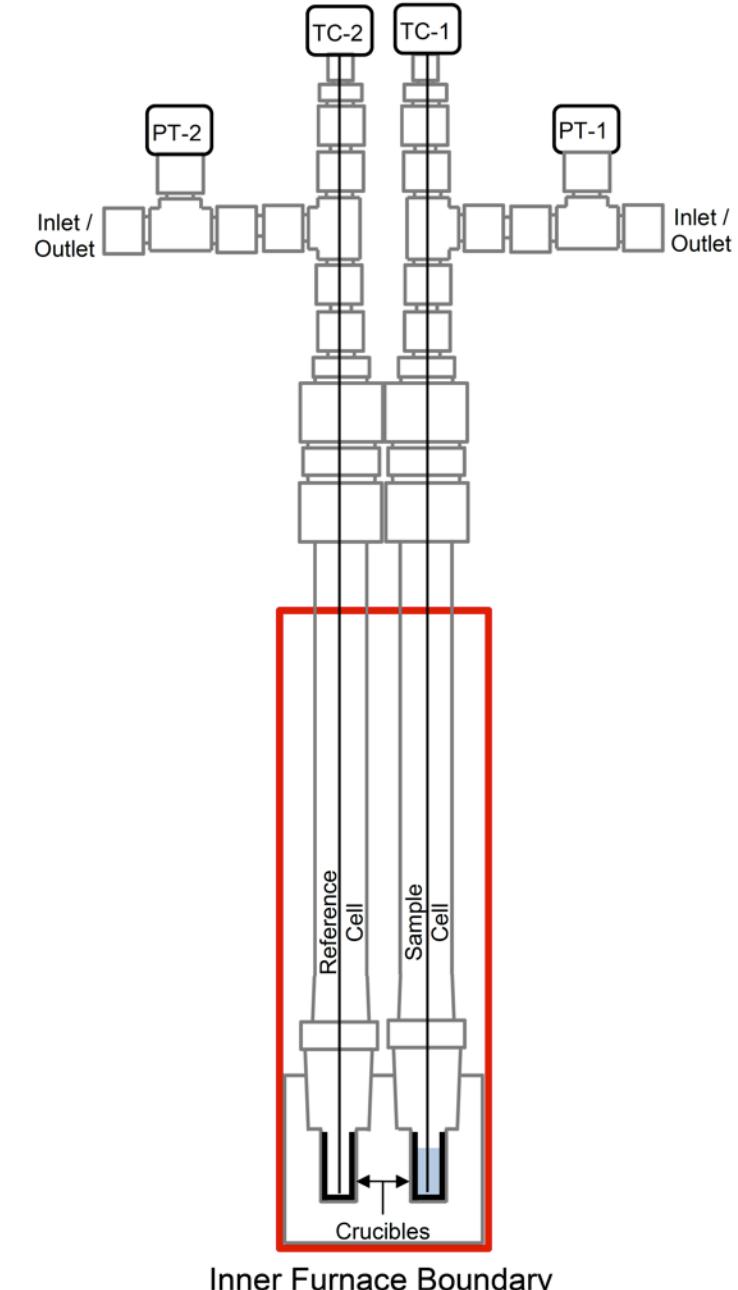
- The combustion of AAN does not require an external oxidizer (i.e.  $\text{O}_2/\text{Air}$ )
- For AAN, the equivalence ratio (the fuel to oxidizer ratio) is as follows:

$$\phi = \text{fuel to oxidizer ratio} / (\text{fuel to oxidizer ratio})_{sto.} = n_{fuel} / n_{oxi.} / 5 / 3$$

- **Hence, fuel rich and lean mixtures correspond to  $\Phi > 1$  and  $\Phi < 1$**

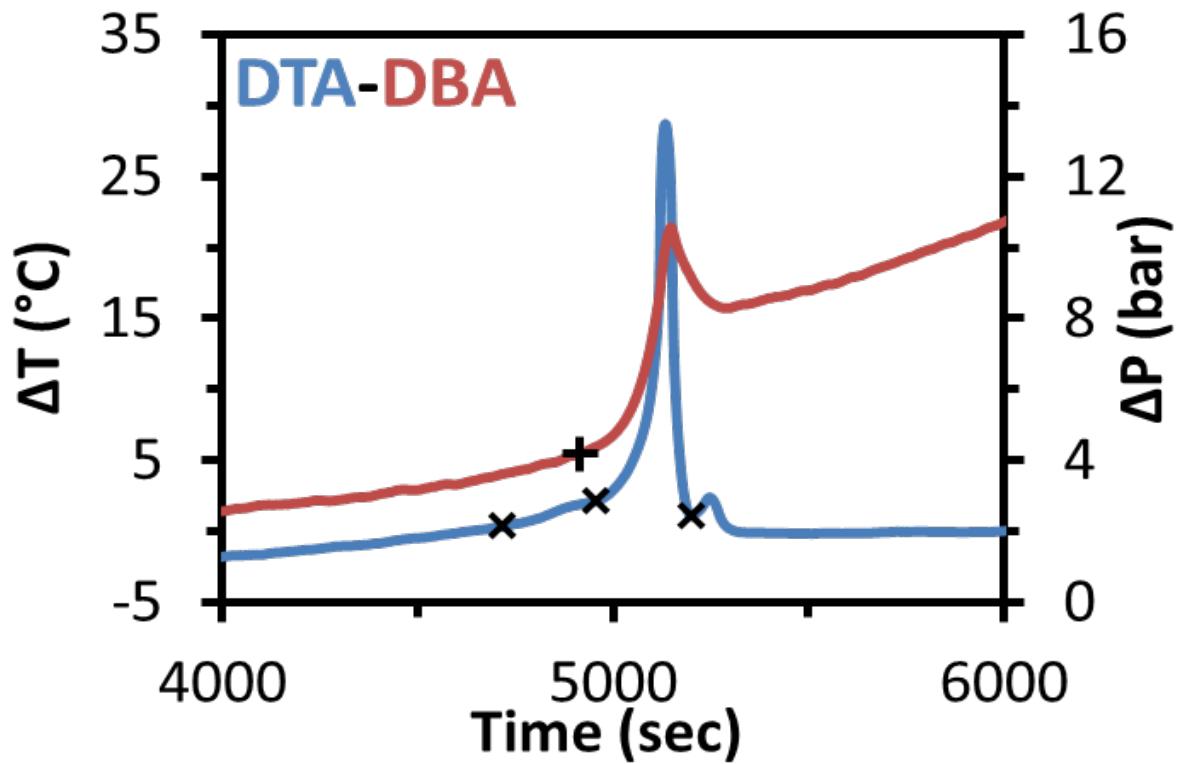
# Experimental

- Testing rig: a dual chamber reactor
- Simultaneous differential thermal / barometric analysis (DTA/DBA)
- Heating  $30^{\circ}\text{C} \rightarrow 450^{\circ}\text{C}$  @  $5^{\circ}\text{C min}^{-1}$
- Parameter of interest: the AIT - the **Auto Ignition Temperature**



A. Grinberg Dana et al., *Fuel*, **159**, 500-507, 2015.

# Autoignition Data



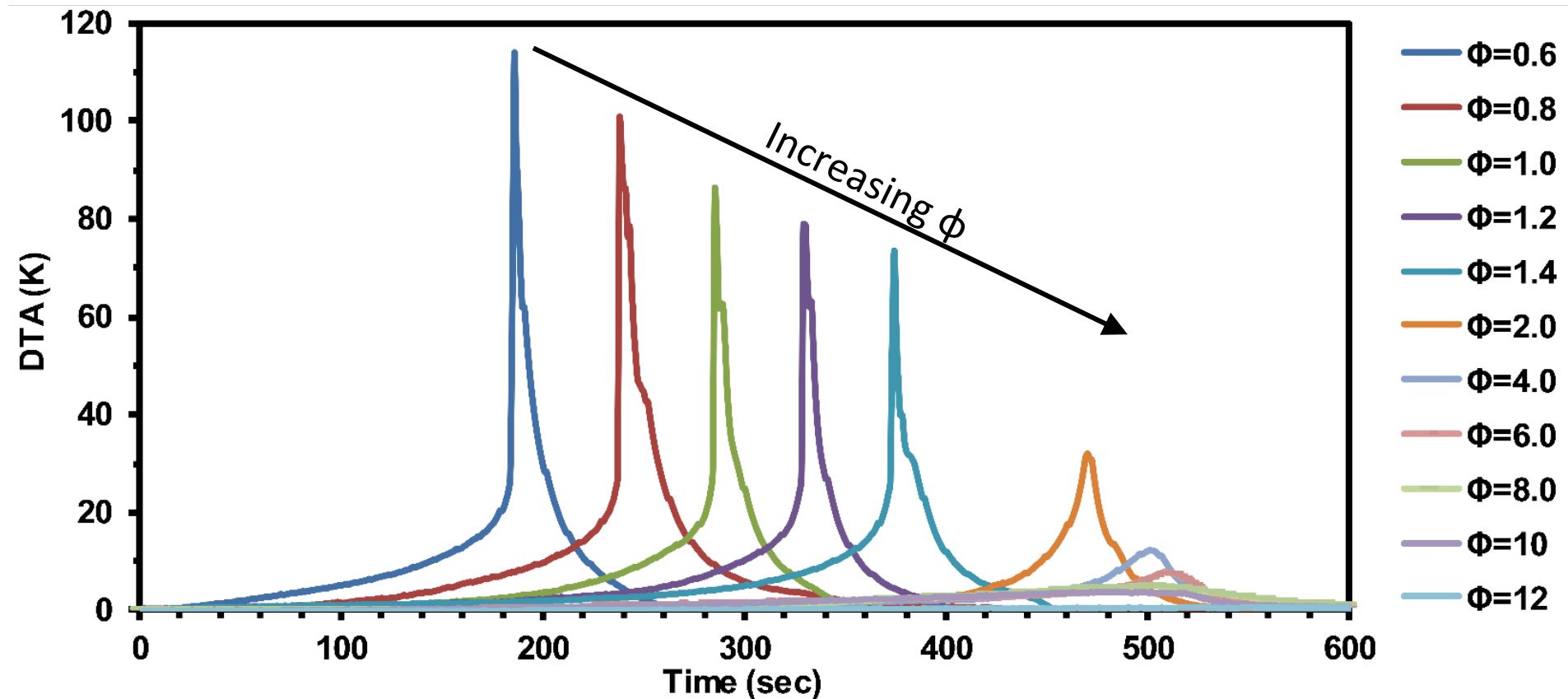
# Effect of $\phi$ on AAN ignition

## $\Delta T$ (K) vs. time starting from 250°C

Increasing  $\phi$ :

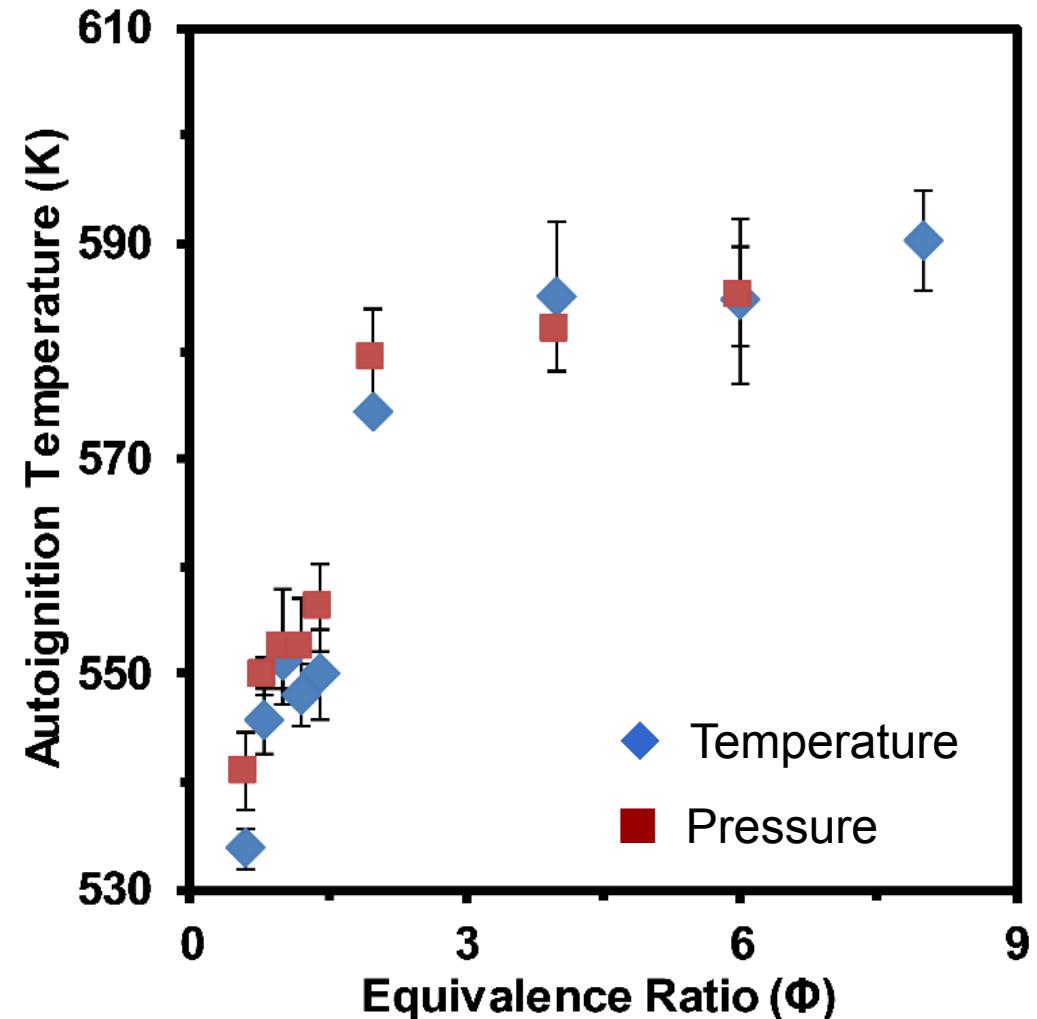
Delays the  
auto ignition

Reduces the  
peak DTA  
value



# Effect of $\phi$ on AAN ignition

- The AIT increased with  $\Phi$
- Autoignition is not detected above  $\Phi=6$  and  $\Phi=8$  using DBA and DTA,
- What happened between  $\Phi=1.6$  and  $\Phi=2.0$

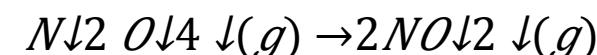
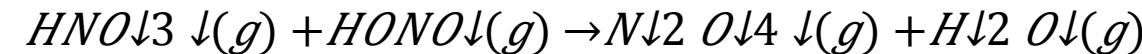


# Effect of $\phi$ on AAN ignition – Reaction Mechanism

- As  $\phi$  is increased, more ammonia is present in the gas phase, thereby increasing the rate of re-formation of AN, and delaying the thermal autoignition:



- Nitric acid mostly reacts to form dinitrogen tetraoxide, which in turn easily decomposes to nitrogen dioxide, generating small amounts of nitrogen trioxide:

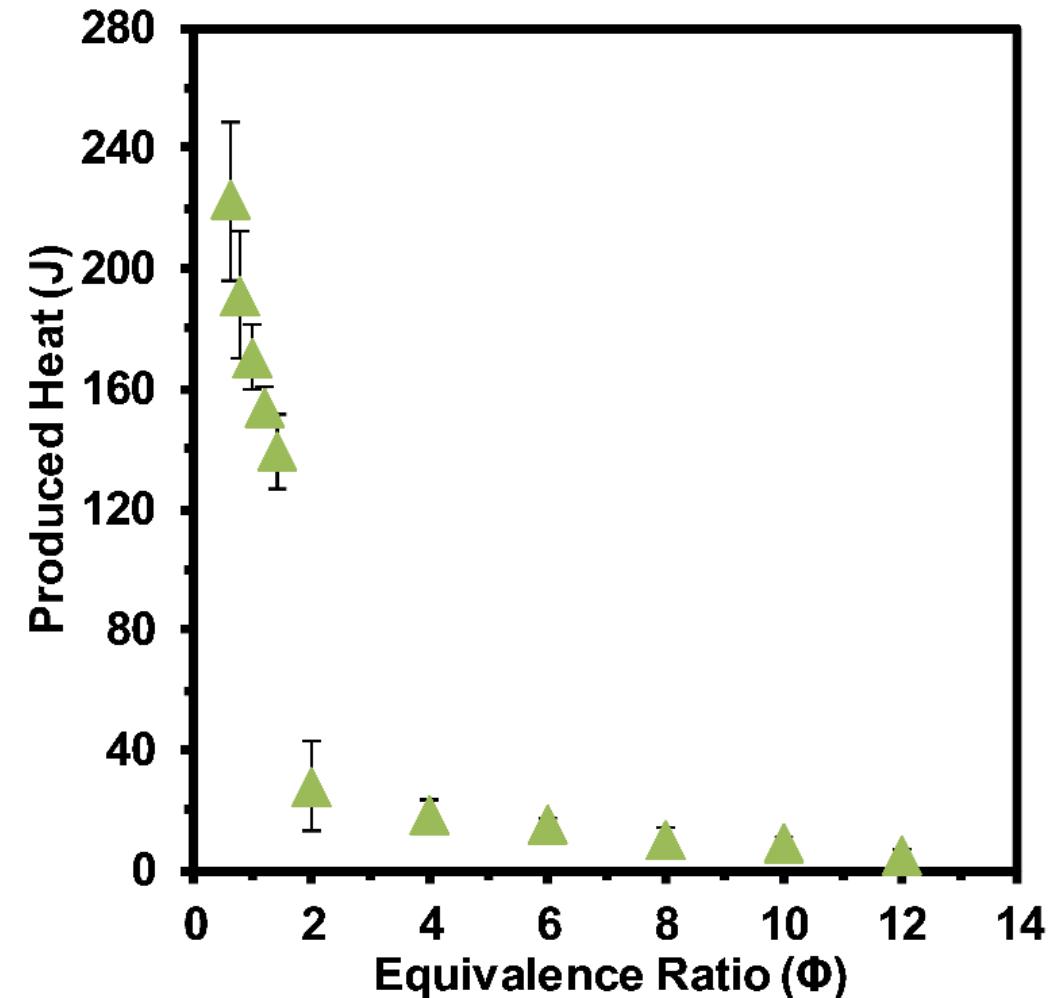


- Since **amidogen generation** is the ignition rate limiting step, higher  $\phi$  values delay the thermal autoignition of AAN:



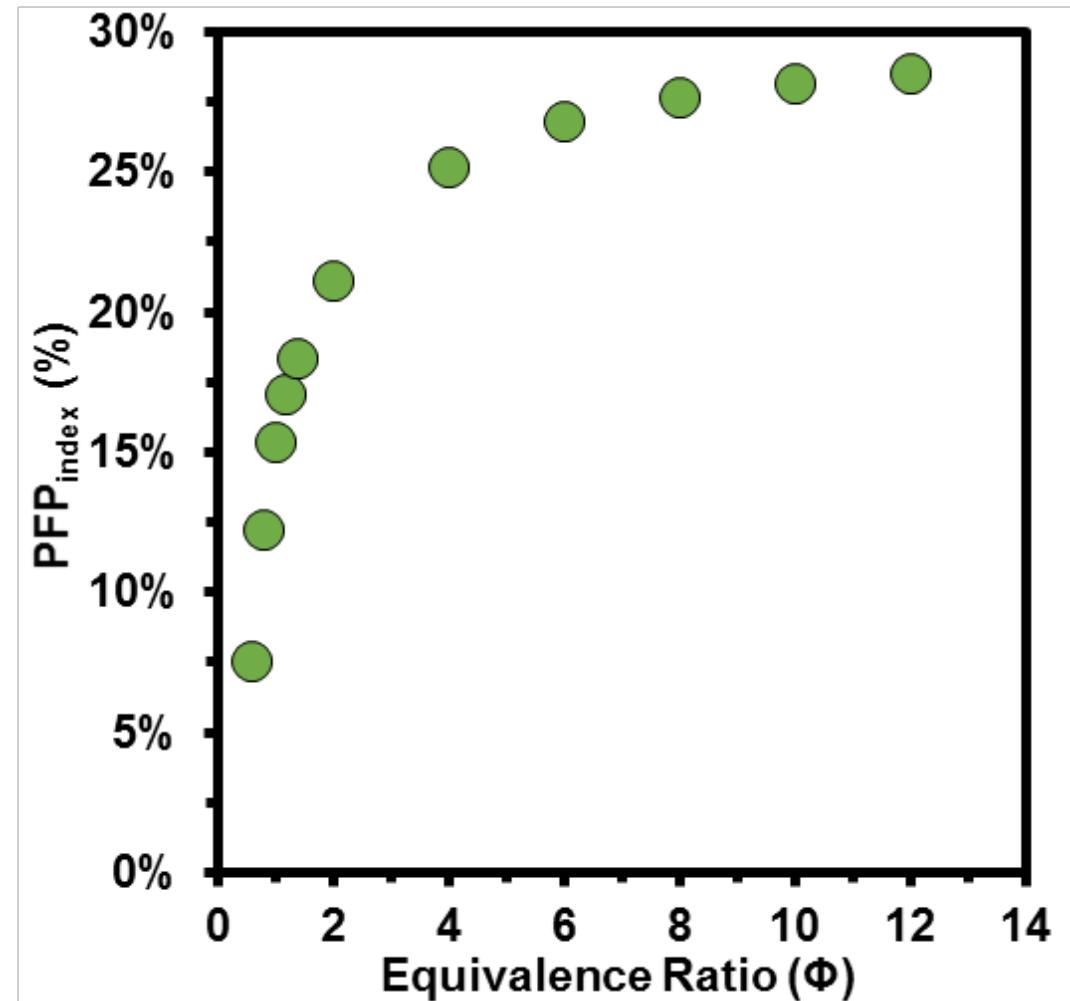
# Effect of $\phi$ on AAN ignition

- The decreasing DTA peaks with increasing  $\Phi$  suggests a smaller exothermic ignition
- To confirm this, the heat produced from 250°C to the ignition peak was calculated
- Generated heat drops with increasing  $\Phi$
- This suggests the ignition is limited by AN content

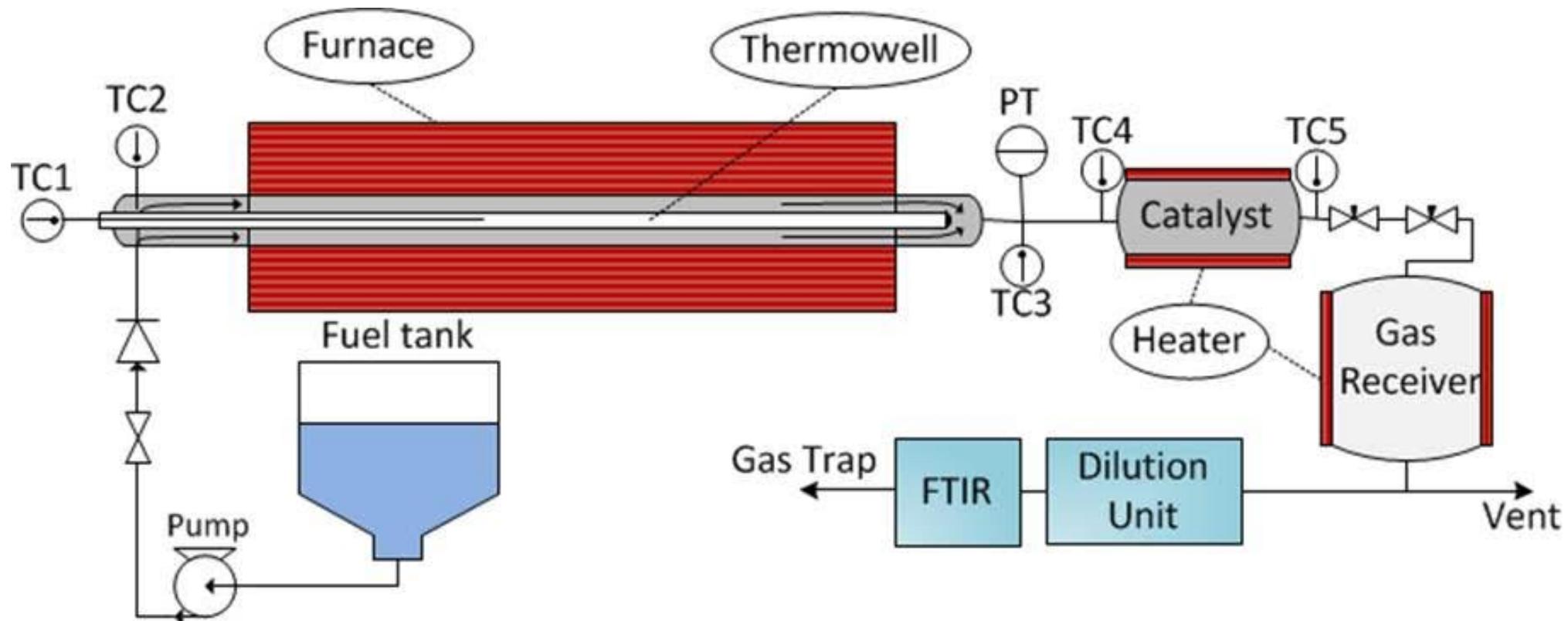


# Effect of $\phi$ on AAN ignition

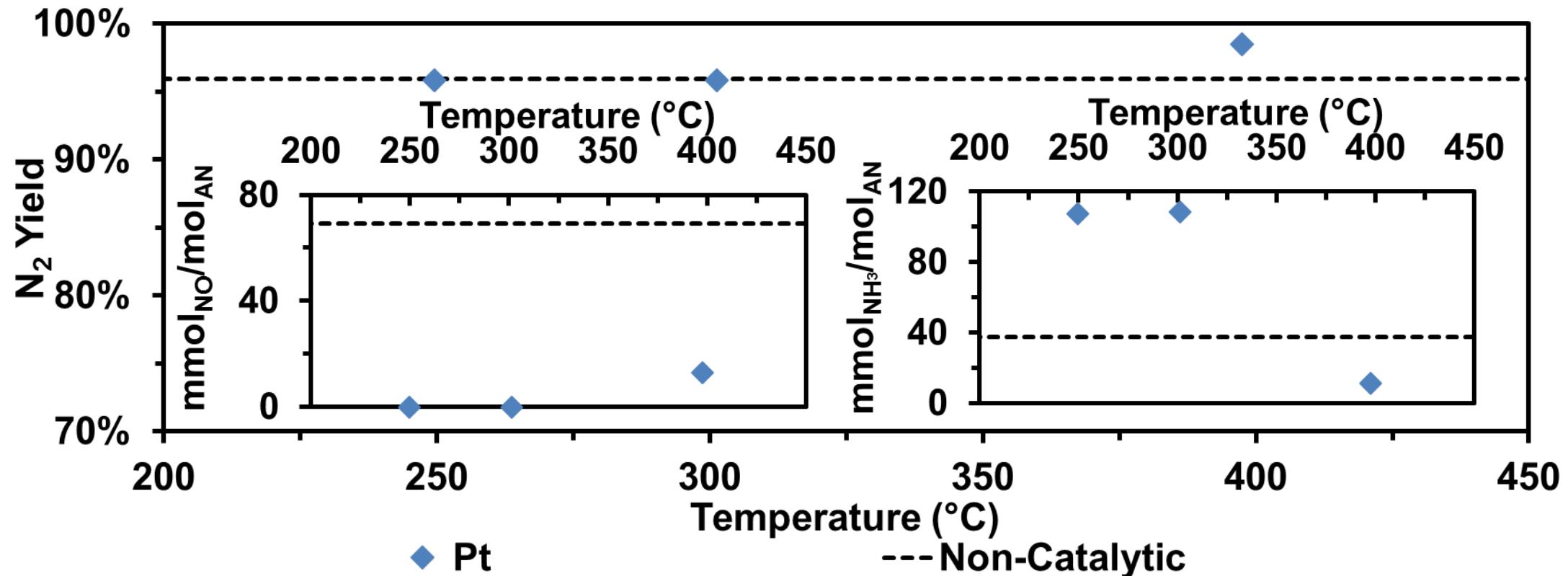
- Increasing large  $\phi$  can lead to higher  $\text{PFP}_{\text{index}}$  if the remaining  $\text{NH}_3$  is oxidized with air.
- Ammonium nitrate can be a catalyst for ammonia ignition at large  $\phi$ .



# Combustion Pollutant Abatement (UAN)

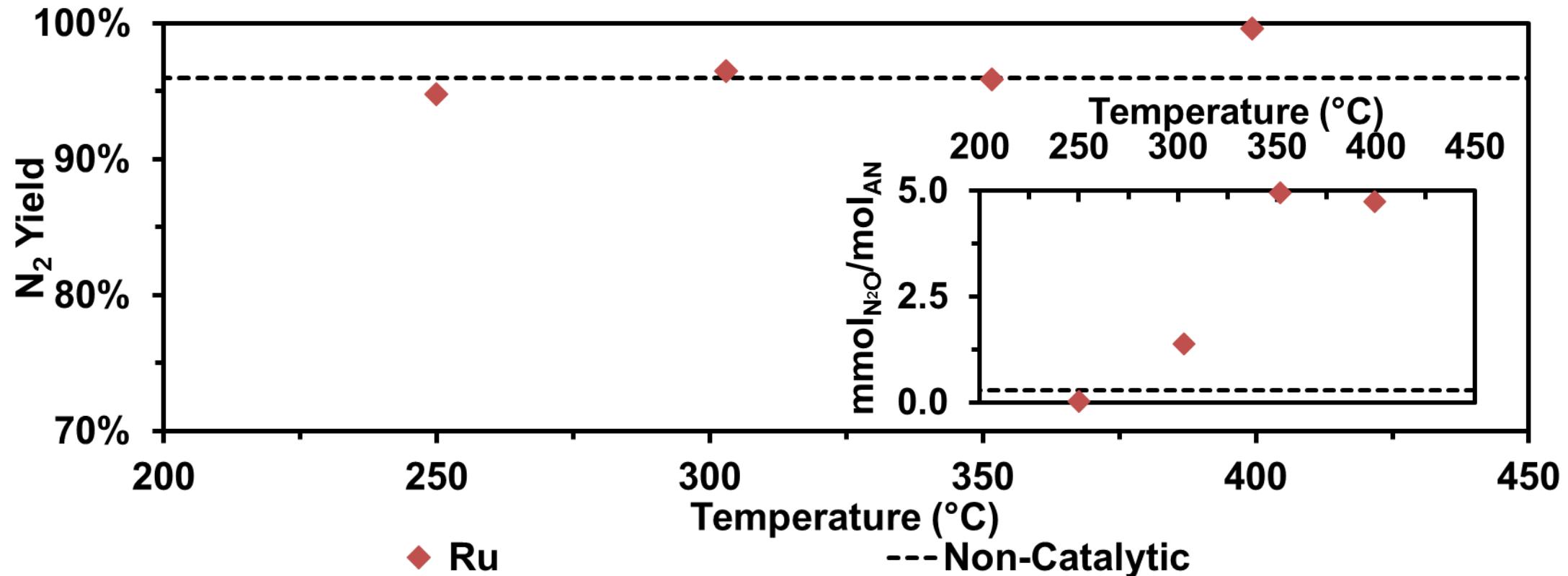


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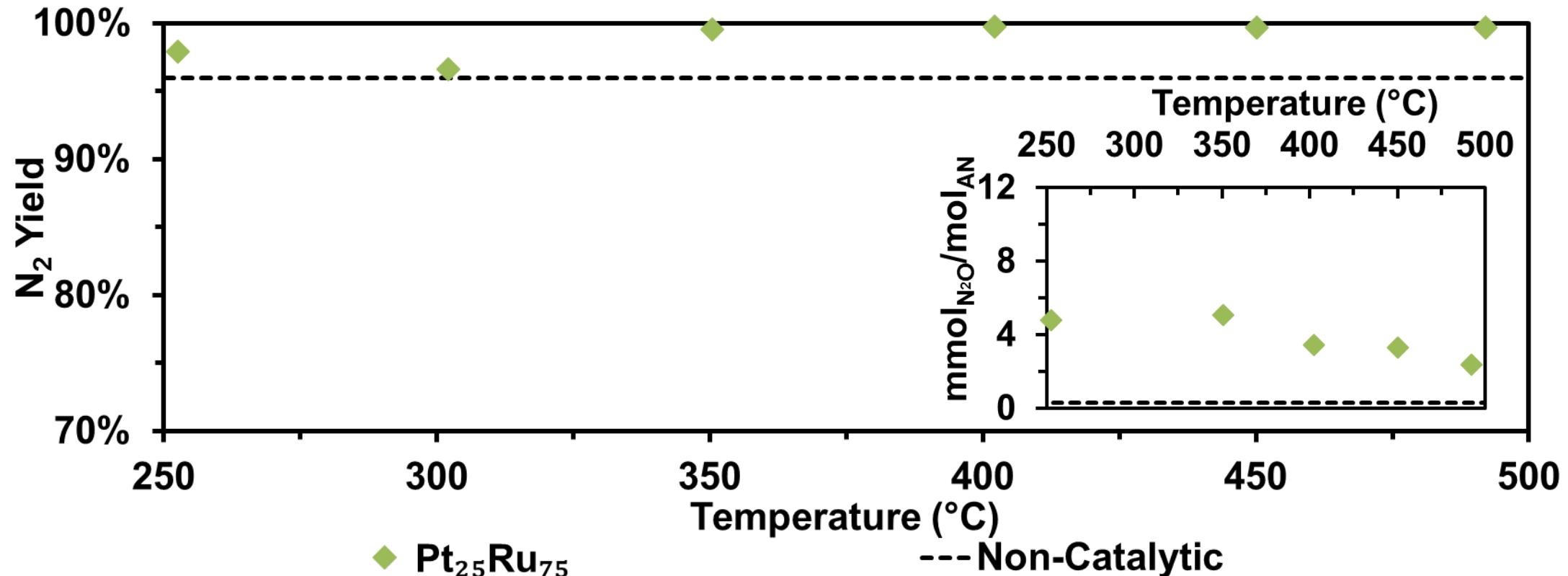
- Platinum can eliminate NO<sub>x</sub> at temperatures as low as 250°C
- But ammonia is generated

# Combustion Pollutant Abatement (UAN)



- Ruthenium shows good pollutant abatement activity only above 350°C
- However, it produces N<sub>2</sub>O rather than NO<sub>x</sub> and ammonia

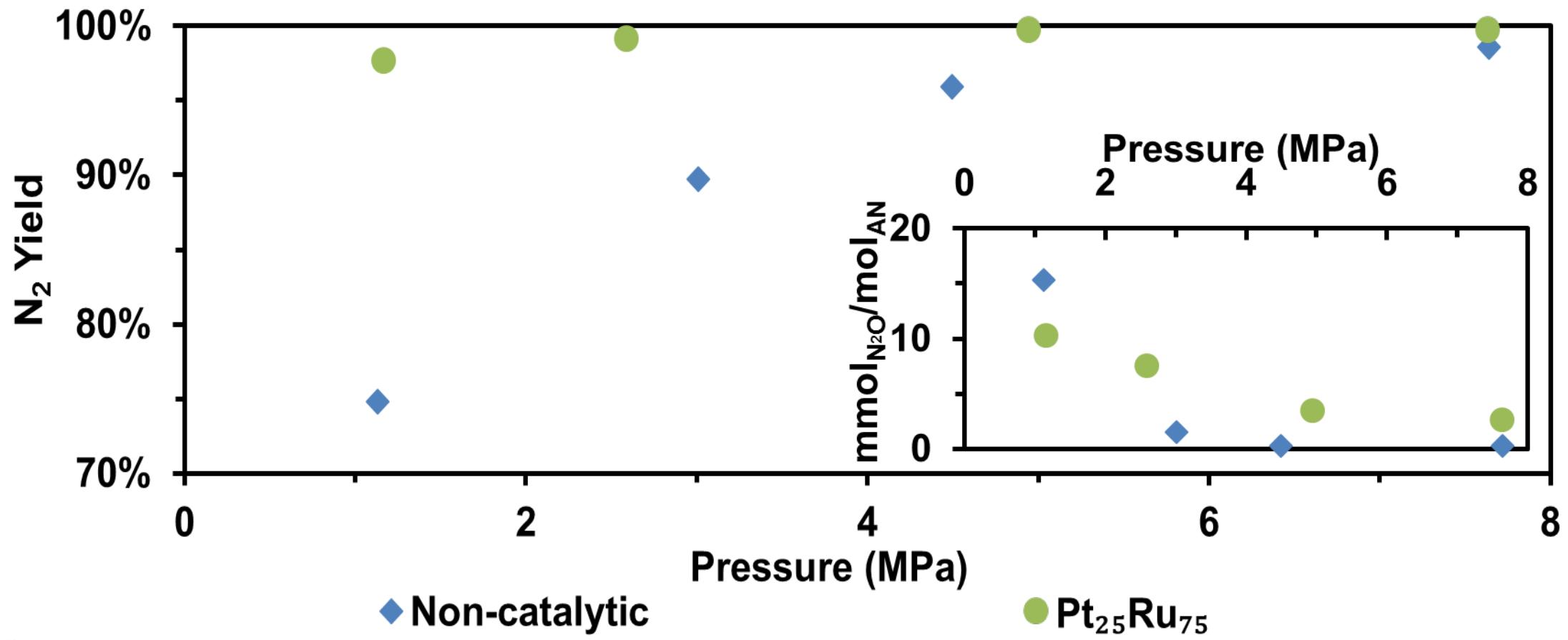
# Combustion Pollutant Abatement (UAN)



- Combining Pt and Ru produces an effect similar to pure Ru
- However, it requires lower temperature (T>300°C) and increases N<sub>2</sub> yield

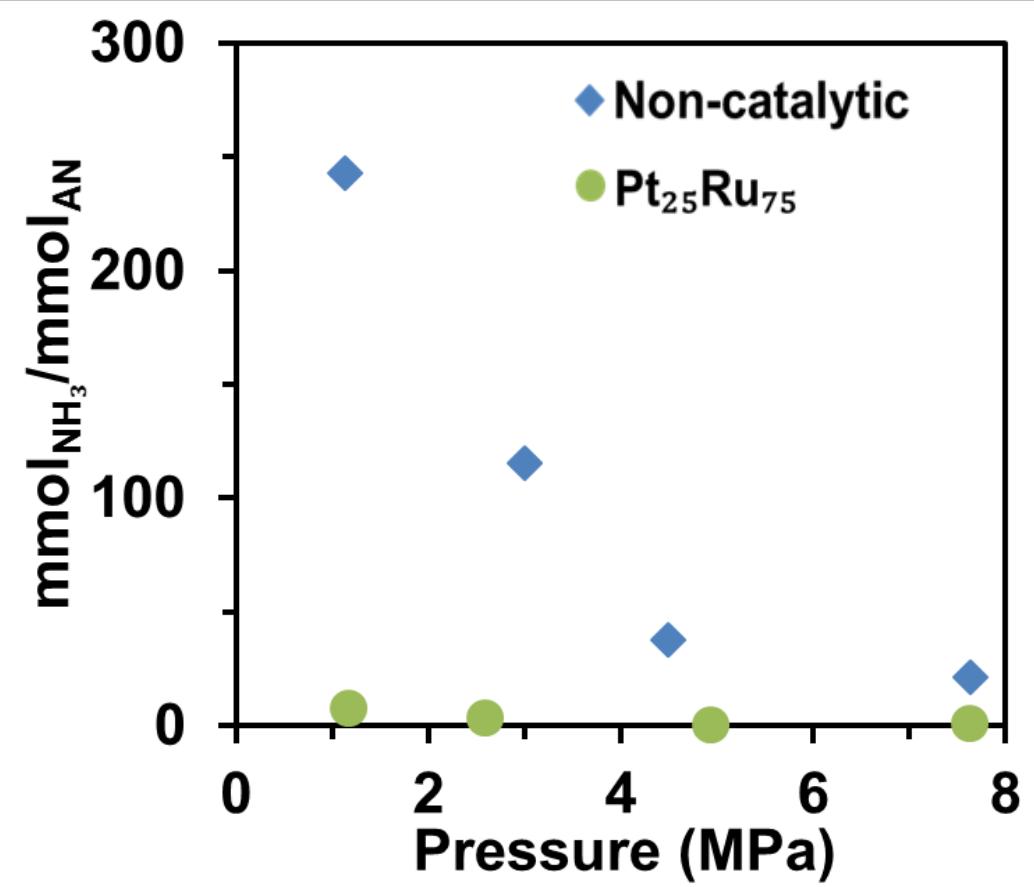
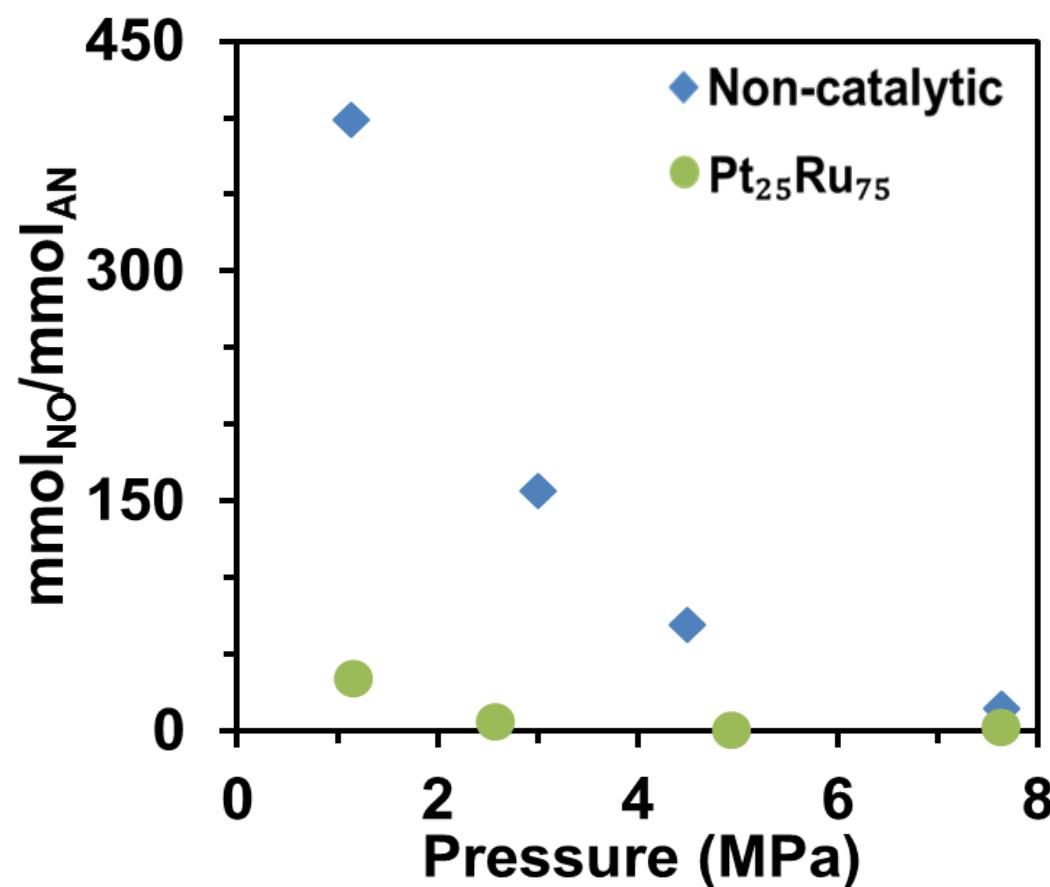
# Combustion Pollutant Abatement (UAN)

With proper catalysts even lower pollutant levels can be reached



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With proper catalysts even lower pollutant levels can be reached



# Conclusions

- PFP index:
  - $\text{NH}_3$  ranks higher than  $\text{CH}_4$ ,  $\text{CH}_3\text{OH}$  or DME on an energy basis
  - UAH (Urea Ammonium Hydroxide) is comparable with HC fuels
  - AN can be used as an initiator for  $\text{NH}_3$  combustion
- The ignition point of AAN increases with Equivalence ratio,
- AN limits the extent of reaction
- Mixed metal catalyst of  $\text{Pt}_{25}\text{Ru}_{75}$  reduces the pollutant emission to a minimum even at 5 MPa



# Acknowledgements



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*Thank you*

